# PASSING \& OVERTAKING ON NEW ZEALAND TWOLANE STATE HIGHWAYS: POLICY TO PRACTICE 

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#### Abstract

A Passing and Overtaking Policy has been formulated to improve the efficiency of New Zealand's two-lane state highway network. The Policy will be applied to two-lane state highways running through rural and peripheral urban land-use areas, up to the point that four-laning is likely to be required. This paper reports on how the Policy was derived and the results of two studies that have contributed to improving implementation of the Policy.

For the passing lane length and frequency study (Cenek \& Lester 2008), six sets of field data were collected using pneumatic dual tube axle sensors located within the passing length and up to 2 km before and 12 km after the passing facility. The operational data acquired was used to refine the Policy's long-term framework for passing and overtaking treatments.

Another study examined the percentage of following vehicles at about 90 rural count stations throughout New Zealand's Waikato and Bay of Plenty areas. For each site, vehicle-by-vehicle and time interval data were used to determine percentage following by direction (Wanty 2007).


Key Words: passing lane, percentage following, platooning, terrain, design criteria

## INTRODUCTION

In October 2006, the Transit New Zealand Board approved its Passing and Overtaking Policy (after 31 July 2008, Transit New Zealand will join with Land Transport New Zealand to form the New Zealand Transport Agency). To implement the Policy, the following approach was taken:

- Routine standardised layout for the majority of sites
- Procedures for dealing with common exceptions
- Data and professional judgement to cater for one-off situations.

A framework of passing lane lengths and frequencies was developed for the majority of sites but needed verification under New Zealand conditions. To help understand one-off situations, a suitable method for measuring passing/overtaking demand was required.

## BACKGROUND

## Terminology

Key words are (may differ slightly from AUSTROADS definitions):

- Passing - vehicles use specific passing facilities to pass slower vehicles.
- Overtaking - vehicles cross into the opposing traffic lane to pass slower vehicles.
- Passing/Overtaking Demand - reflects both the amount of traffic bunching and the desire for following vehicles to pass or overtake slower moving vehicles.
- Treatments - are applied directly to the roading infrastructure.
- Measures - act on driver behaviour.


## Projected Flows

Table 1 shows the traffic flows on lengths of New Zealand rural two-lane state highways. The projected traffic volumes have been derived from work undertaken for the National State Highway Strategy (Transit New Zealand 2007). As a comparison, the New Zealand state highway network is currently about $11,000 \mathrm{~km}$ long.

Table 1. Estimated Current \& Projected Flows.

| AADT (vpd) | Current (2006) (km) | Next 25-30 Years (km) |
| :--- | :---: | :---: |
| $\mathbf{1 2 , 0 0 0} \mathbf{- 2 5 , 0 0 0}$ | 200 | $\mathbf{1 , 1 0 0}$ |
| $\mathbf{4 , 0 0 0 - 1 2 , 0 0 0}$ | 2,300 | 3,200 |
| $\mathbf{4 , 0 0 0}$ | 7,400 | 5,600 |
| Total | $\mathbf{9 , 9 0 0}$ | $\mathbf{9 , 9 0 0}$ |
| Note: Does not include state highway sections in urban zones or rural sections identified for four-laning. |  |  |

An additional 900 km of state highway is expected to have 12,000-25,000 vpd. This flow range usually suits four-laning but an intermediate $2+1$ lane layout (continuous alternating passing lanes) will now be considered, subject to a four-lane comparison.

The 4,000-12,000 vpd range is usually suitable for passing lanes in series. The length of state highway within this range is expected to increase by about $40 \%$. About $56 \%$ of New Zealand two-lane state highways would still have less than $4,000 \mathrm{vpd}$, with most of this length suitable for an overtaking strategy.

## PREVIOUS RESEARCH

Prior to developing its Passing and Overtaking Policy, Transit prepared a background technical report, which reviewed both New Zealand and overseas research (Transit New Zealand 2006).

New Zealand research from 1996-2003 looked at a variety of operational and safety issues relating to two-lane state highways (Thrush 1996), (McLarin 1997), (Tate 1997), (Koorey et al, 1999), (Koorey \& Gu 2001). Before project evaluation procedures for passing lanes and slow vehicle bays were introduced in 2001, a report was commissioned by Transit New Zealand (Bone \& Turner 2000). Subsequent research has looked at improvements to these procedures (Koorey \& Gu 2001), (Koorey, 2003), (Roozenburg \& Nicholson 2004).

Most overseas research into passing lanes has been based in North America and is summarised in later US studies (Mutabazi, Russell \& Stokes 1999). Relevant research involved operational efficiency and safety (Harwood, St John \& Warren 1985), optimum passing lengths and downstream effective lengths, cost effective methods for two-lane state highways (Harwood \& Hoban 1987) and measuring level of service on two-lane state highways (Morrall \& Werner 1990).

South African research has used follower density as a measure of network passing demand (South African National Roads Agency Ltd 2004). Measuring demand over a network was of particular interest to the New Zealand situation. Some New Zealand and US research was used to establish a survey methodology (Koorey \& Gu 2001), (Harwood, St John \& Warren 1985).

## POLICY

## Types of Strategy

Projected traffic flows and road gradients can be loosely grouped into four different types of strategy, as shown in Table 2.

Table 2: Summary of Passing \& Overtaking Strategy Types

| Strategy Types | Summary of Passing and Overtaking Treatments | Typical 25-30 Year Projected Traffic Flow Where Each Strategy Type Applies (vpd) |  |
| :---: | :---: | :---: | :---: |
|  |  | Flat Road Gradient | Rolling or Mountainous Road Gradient |
| Overtaking | - Sight distance improvements <br> - Overtaking enhancements <br> - Possibly, isolated short passing lanes, slow vehicle bays (SVBs), shoulder widening or crawler shoulders. | Less than 4,000 | Less than 2,000 |
| Mainly Overtaking | - Sight distance improvements <br> - Overtaking enhancements <br> - Possibly, some "in series" (i.e. regular and frequent) short passing lanes, slow vehicle bays (SVBs), shoulder widening or crawler shoulders. | 4,000-5,000 | 2,000-4,000 |
| Passing \& Overtaking | - In series passing lanes <br> - Overtaking enhancements <br> - Crawler lanes where appropriate. | 5,000-12,000 | 4,000-10,000 |
| Passing | - 2+1 lanes on flat/rolling road gradients (subject to comparison with four-lanes) <br> - Passing lanes in series on mountainous road gradients <br> - Crawler lanes where appropriate. | 12,000-25,000 | 10,000-25,000 |

Note: A range of supporting treatments and measures are also applied, depending on strategy type. See Fig 1.

## Long - Term Framework

Passing and overtaking treatments have been further refined into long-term layouts, as shown in Table 3. Further improvements are discussed within sections of this paper headed Verification of Policy Framework and Conclusions. Table 3 key and notes are provided overleaf.

Table 3. Long-Term Framework for Passing \& Overtaking Treatments

| Projected AADT (vpd) | Road Gradient |  |  |
| :---: | :---: | :---: | :---: |
|  | Flat | Rolling | Mountainous |
| <2,000 | Overtaking (OT) (OT sight distance improvements, OT enhancements, possible isolated shoulder widening/crawler shoulder/SVBs¹/short PLs). |  |  |
| 2,000-4,000 | Overtaking (As above). | Mainly OT, as above but possibly some SVBs ${ }^{1}$ or short PLs @ 10 km. |  |
| 4,000-5,000 (General transition to PLs) | Mainly OT, as above but possibly some SVBs ${ }^{1}$ or short PLs @ 10 km. | PLs @ 10km $1.2 \mathrm{~km}+$ tapers \& OT enhancements. | PLs @ 5 km $1.0 \mathrm{~km}+$ tapers \& possible OT enhancements. |
| 5,000-7,000 ${ }^{3}$ | PLs ${ }^{2} @ 5$ or 10 km $1.2 \mathrm{~km}+$ tapers <br> \& OT enhancements. |  |  |
| 7,000-10000 | PLs ${ }^{2}$ @ 5 or 10 km 1.5 km + tapers \& OT enhancements. |  | PLs @ 5 km $1.2 \mathrm{~km}+$ tapers \& possible OT enhancements. |
| 10,000-12,000 (General transition to $2+1$ lanes) | PLs @ 5 km $1.5 \mathrm{~km}+$ tapers \& possible OT enhancements | 2+1 lanes (subject to four-lane comparison). | PLs @ 5 km 1.2-1.5 km + tapers. |
| 12,000-20,000 | 2+1 lanes (subject to four-lane comparison). |  |  |
| 20,000-25,000 (General transition to 4 lanes) |  |  |  |


| Key - Strategy <br> Type | Overtaking | Mainly overtaking | Passing and <br> overtaking | Passing |
| :--- | :--- | :--- | :--- | :--- |

Notes: 1. Where appropriate, a SVB is able to be easily altered to a short PL or PL at a later date.
2. Along the same road section, a mixed layout with 5 km spacing in higher demand locations and 10 km spacing in lower demand locations.
3. For flat or rolling road gradient, the combination of passing lane length and spacing may not be sufficient to dissipate vehicle queues and a more frequent provision of passing opportunities would be required. Therefore, passing treatments, such as $2+1$ lanes (subject to comparison with four-lanes), are likely to be required for state highways with a flat or rolling gradient and projected 10,000-25,000 vpd.
4. 10,000-12,000 vpd represents a general upper limit for passing lanes in series with flat or rolling gradient. Above this threshold, treatments such as $2+1$ lanes (subject to comparison with four-lanes), are likely to be required. Some locations may have a higher upper limit of about 14,000 vpd depending on other factors, such as the directional flow split and traffic composition.

The Policy uses projected AADT and road gradient (vertical alignment) as primary influences of passing/overtaking demand. However, as other influences will affect passing/overtaking demand, some flexibility is required when applying the long-term framework.

## Integration of Treatments and Measures

Both passing and overtaking treatments are supported by a number of other treatments and measures. Table 4 suggests a range of treatments and measures for each strategy. A tool-kit of preferred options (Appendices, Figure 1) subdivides Table 4 further so that preferred option/s within each treatment and measure can be identified.

Table 4. Integration of Treatments \& Measures

| Category of Treatment or Measure | Passing and Overtaking Strategy |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Overtaking | Mainly Overtaking | Passing \& Overtaking | Passing |
| Overtaking Treatments |  |  |  |  |
| OT sight distance improvements | C | C | C | - |
| OT enhancements | A | A | A | - |
| Passing Treatments |  |  |  |  |
| Low-volume treatments | A* | A* | - | - |
| Moderate-volume treatments | - | - | A | A |
| Supporting Treatments |  |  |  |  |
| Centreline | A | A | A | A |
| Roadside and edgeline | A | A | A | A |
| Intersections | C | C | A | A |
| Supporting Measures |  |  |  |  |
| Resource Planning | C | C | A | A |
| Education | C | C | C | A |
| Enforcement | C | C | C | A |
| TDM | C | C | C | A |
| ITS | C | C | C | C |

Notes: A means apply. A* means apply if overtaking is not viable.
C means consider if potential or actual problem

## VERIFICATION OF POLICY FRAMEWORK

## Methodology

Five passing lanes and one slow vehicle bay were surveyed by Opus International Consultants Ltd. Site details are summarised in Table 5. The percentage of light vehicle towing and heavy commercial vehicles (LVT and HCV) tabulated in Table 5 is the average of the busier daytime ( 7 am to 8 pm ) flows for each day over the survey period of 3 weekdays.

Table 5: Details of Surveyed Sites

| Type | Site ID | SH | Location | Length (m) | D/stream Road Gradient ${ }^{1}$ (\%) | Average Grade along PL/SVB (\%) | Flows (3 day) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | ADT (vpd) | LVT + HCV $^{2}$ (\%) |
| $\begin{aligned} & \text { Short } \\ & \text { PL } \end{aligned}$ | 2 e | 57 | 0/15.80-15.16 | 599 | R (0-3) | M (6.8) | 6,200 | 10 |
|  | 3 e | 1N | 680/0.56-1.11 | 556 | M ( $>6$ ) | R (5.7) | 5,000 | 19 |
| Long PL | 4j | 3 | 450/13.3-14.25 | 939 | F (<3) | F (0.4) | 9,200 | 6 |
|  | $5 f$ | 1 N | 574/11.88-10.36 | 1,397 | $\mathrm{R}(3-6)$ | F (0.3) | 11,400 | 18 |
|  | 6 e | 58 | 0/1.09-2.27 | 1,192 | M ( $>6$ ) | M (7.2) | 13,600 | 10 |
| SVB | 8j | 5 | 11/9.90-9.70 | 325 | M ( $>6$ ) | M (6.4) | 3,200 | 15 |

Notes: 1. F=flat, R=rolling, M=mountainous road gradient.
2. LVT + HCV percentages relate to the average value during peak hourly flows.

Except for site 4 j , sites were selected so that the 2 km before and the $10-15 \mathrm{~km}$ after each passing facility was free of major roadside roads, one-lane bridges and railway crossings. The passing facilities were located away from major settlements and free of both turning bays and major egress points to properties. The absence of these features helped to ensure that secondary effects did not confound the percentage following results. It was later discovered that site 4 j was a mobile speed camera site, which is a likely influence on the site's poor performance. Figure 2 shows the counter layout adopted for the passing facilities surveyed. MetroCount ${ }^{\text {TM }}$ Plus 5600 pneumatic counters were used to survey three weekdays of vehicle-by-vehicle percentage following and speed data as well as hourly flows in each direction by vehicle class. The study period was from Tuesday 10/7/2007 to Friday 27/7/2007.

## Percentage of Vehicles Following

For the six study sites, immediately downstream of the passing facility and based on a 4 seconds headway criterion, the surveyed reduction in percentage of vehicles following was on average 4.4 percent. This is comparable to the 5.9 percent measured by Harwood et al. (1985) over similar average traffic flows ( 35 to 560 vehicles per hour one-way) at 12 passing lane and 3 short four-lane sites.

As an indicator of influential variables, regression analysis identified the following model, which was the best fit for the hourly passing lane data when aggregated into 50 vph bands and averaged.

$$
\begin{gathered}
\Delta \mathrm{PF}=-69.98+5.70 \ln (\mathrm{LEN})+0.128 \mathrm{FLOW}+\frac{1688}{\mathrm{FLOW}}+18.2 \ln (\mathrm{UPF})-0.03 \times \mathrm{FLOW} \times \ln (\mathrm{UPF}) \\
+0.29 \mathrm{GPL}-0.09 \mathrm{LTHV} \ldots(1) \\
\left(\mathrm{r}^{2}=0.45, \mathrm{SE}=1.6 \%, \text { no. of observations }=32\right)
\end{gathered}
$$

where: $\quad \Delta \mathrm{PF}=$ difference in percentage vehicles delayed upstream and downstream of the passing lane based on 4 seconds headway criterion.
LEN = length of the passing lane (km).
FLOW = traffic flow rate in treated direction (FLOW $\leq 700 \mathrm{vph}$ ).
UPF = percentage of vehicle delayed upstream of the passing lane.
GPL = average gradient along passing lane (\%).
LTHV = percentage light towing and heavy vehicles in the traffic stream.
Equation 1 has the same form as proposed by Harwood et al (1987) from results of 85 computer simulation runs, but with the addition of average grade along the passing lane (GPL) and percentage light towing and heavy vehicle (LTHV) variables. It illustrates the complexity of the relationships and interactions that influence a passing facility's effectiveness. The most significant predictor variables (p-value < 0.05 ) were $\ln (\mathrm{LEN}), \ln (\mathrm{UPF})$ and GPL.

## Downstream Operational Length

Percentage following was used to help determine the downstream operational length. This downstream length is the distance from the end of the merge taper through to where percentage following matches surveyed values immediately upstream of the passing facility.

Using raw hourly data, Table 6 shows the estimated average downstream operational length and range relative to one-way flow. The 2 second results had a larger reduction in percentage following after the passing lane or slow vehicle bay and were a better indicator of platooning effects. The downstream percentage following eventually reaches the same value as immediately before the passing facility.

Table 6: Estimated Downstream Operational Length Based on Survey Data

| Site | Range of Downstream Road Gradient ${ }^{1}$ (\%) | Observed One-Way <br> Flow (vph) | Observed HCV+LVT <br> (\%) | Headway (sec) | Estimated Downstream Operational Length (km) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Average | Range |
| 2 e | $\mathrm{R}(0-3)$ | $\geq 260$ | 8-13 | 4 | PL ineffectual |  |
|  |  | 261-328 | 8-13 | 2 | 6.8 | 4.1-11 |
| 3 e | M ( $>6$ ) | $\geq 190$ | 17-21 | 4 | PL ineffectual |  |
|  |  | 190-250 | 17-21 | 2 | 10.0 | 6.4-13.7 |
| 4j | F (<3) | 343-487 | 5-10 | 4 | 6.7 | 3.8-11.1 |
|  |  |  |  | 2 | 13.5 | 3.4-21.7 |
| $5 f$ | R (3-6) | 355-558 | 13-20 | 4 | 4.8 | 2.7-9.7 |
|  |  |  |  | 2 | 6.9 | 3.4-12.8 |
| 6 e | M ( $>6$ ) | $\geq 688$ | 7-13 | 4 | PL ineffectual |  |
|  |  | 693-805 |  | 2 | 3.9 | 1.3-5.4 |
| 8j | M ( $>6$ ) | $\geq 148$ | 12-19 | 4 | SVB ineffectual |  |
|  |  | 170-192 | 14-15 | 2 | 2.4 | 1.2-3.6 |
|  |  | 114-143 | 12-18 | 2 | 8.4 | 3.5-14.5 |

Note. 1. $\mathrm{F}=$ flat, $\mathrm{R}=$ rolling, $\mathrm{M}=$ mountainous road gradient.
The general pattern is that downstream operational length reduces with increasing flow, \%HCV+LVT and downstream gradient, which is to be expected. At lower flows, for passing lanes, a shorter operational length for the 2 seconds headway criterion was obtained and was unexpected. This pattern may be due to a lower proportion of vehicles with 2 seconds or less headway at lower flows. Therefore, the smaller proportion of following vehicles was possibly more sensitive to downstream conditions. Further investigation would be required to confirm this possible explanation. For each site, Figure 3 shows the variation in upstream and downstream percentage following for 2 seconds headway with zero distance being the start of the facility.

As an indicator of important variables, regression modelling applied to estimated operational lengths derived on 2 seconds headway percentage following distributions, yielded the following model:

$$
\begin{gathered}
\mathrm{OL}=21.39-0.017 \mathrm{FLOW}-(212 / \mathrm{DPF})-0.002 \mathrm{LTHV}+0.04 \mathrm{GDS} \\
\left(\mathrm{r}^{2}=0.77, \mathrm{SE}=1.48 \mathrm{~km}, \text { no. of observations }=14\right)
\end{gathered}
$$

where: $\quad \mathrm{OL}=$ downstream operational length $(\mathrm{km})$.
FLOW = flow rate in treated direction ( $100 \mathrm{vph} \leq \mathrm{FLOW} \leq 700 \mathrm{vph}$ ).
DPF = percent vehicles delayed immediately downstream of passing lane ( $11 \% \leq$ DPF $\leq 40 \%$ ).
LTHV $=$ percentage light towing and heavy vehicles (5\% $\leq$ LTHV $\leq 20 \%$ ).
GDS = nominal downstream road gradient in \% (flat $=1.5 \%$, rolling $=4.5 \%$ and mountainous $7.5 \%$ ).

The most significant predictors ( p -value < 0.05) were FLOW and 1/DPF. For the regression modelling, the raw hourly data have been aggregated into 50 vph bands and the average of each band used as the variable.

Further research is needed to calculate the effects of gradient and percentage of light towing and heavy vehicles. The sign for GDS is positive and therefore intuitively wrong. However, both GDS and LTHV do not contribute markedly to the operational length value. Possibly, downstream gradient and overtaking conditions relative to opposing flows have to be more accurately determined. The equation form for operating length may not be conducive for modelling LTHV effects, which are influenced by terrain. For example, on flat terrain all LTHV values are expected to have little influence on operational length.

## Comparison with Policy Framework

Table 7 compares the difference between the Policy and estimated operational lengths. High traffic flow rates were used with a 2 seconds headway criterion to match peak flow conditions. Observed results are on top and not bracketed. Policy values are underneath and bracketed.

Table 7: Comparison between Observed \& Policy Layouts (2 second headway)

| Site Details |  |  | Flow Characteristics |  | Layout |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site | PL/SVB Gradient (\%) | D/stream Gradient (\%) | LVT \& HCV (\%) | Projected AADT Interval (vpd) | PL or SVB Length (km) | Downstream Operational Length (km) |
| 2e | $\begin{gathered} 6.8 \\ (0-3) \end{gathered}$ | $\begin{gathered} 0-3 \\ (0-3) \end{gathered}$ | $\begin{gathered} 8-13 \\ (<20) \end{gathered}$ | $\begin{aligned} & 4,500-5,700 \\ & (4,000-5000) \\ & (5,000-7000) \end{aligned}$ | $\begin{gathered} 0.6^{1} \\ (0.6-0.8) \\ (1.2) \end{gathered}$ | $\begin{gathered} 7 \\ (10) \\ (5 \text { or } 10)^{2} \end{gathered}$ |
| 3 e | $\begin{gathered} 5.7 \\ (>6) \end{gathered}$ | $\begin{gathered} >6 \\ (>6) \end{gathered}$ | $\begin{aligned} & 17-21 \\ & (<20) \end{aligned}$ | $\begin{gathered} 3,300-4,300 \\ (2,000-4,000) \end{gathered}$ | $\begin{gathered} 0.6 \\ (0.6-0.8) \end{gathered}$ | $\begin{gathered} 10 \\ (10) \end{gathered}$ |
| 4j | $\begin{gathered} 0.4 \\ (0-3) \end{gathered}$ | $\begin{gathered} 0-3 \\ (0-3) \end{gathered}$ | $\begin{gathered} 5-10 \\ (<20) \end{gathered}$ | $\begin{gathered} 4,400-6,200 \\ (4,000-5,000) \\ (5,000-7,000) \end{gathered}$ | $\begin{gathered} 0.9 \\ (0.6-0.8) \\ (1.2) \end{gathered}$ | $\begin{gathered} 8^{3} \\ (10) \\ (10) \end{gathered}$ |
| $5 f$ | $\begin{gathered} 0.3 \\ (3-6) \end{gathered}$ | $\begin{gathered} 3-6 \\ (3-6) \end{gathered}$ | $\begin{aligned} & 13-20 \\ & (<20) \end{aligned}$ | $\begin{gathered} 6,100-9,700 \\ (7,000-10,000) \end{gathered}$ | $\begin{gathered} 1.4 \\ (1.5) \end{gathered}$ | $\begin{gathered} 7 \\ (5 \text { or } 10) \end{gathered}$ |
| 6 e | $\begin{gathered} 7.2 \\ (>6) \end{gathered}$ | $\begin{gathered} >6 \\ (>6) \end{gathered}$ | $\begin{gathered} 7-13 \\ (<20) \end{gathered}$ | $\begin{gathered} 10,500-12,200 \\ (10,000-25,000) \end{gathered}$ | $\begin{gathered} 1.2 \\ (1.2-1.5) \end{gathered}$ | $\begin{gathered} 4 \\ (5) \end{gathered}$ |
| 8j | $6.4$ $(>6)$ | $>6$ $(>6)$ | $\begin{aligned} & 14-15 \\ & 12-18 \\ & (<20) \end{aligned}$ | $\begin{gathered} 2,900-3,300 \\ 2,000-2,500 \\ (2,000-4,000) \end{gathered}$ | $\begin{gathered} 0.33 \\ 0.33 \\ (0.6-0.8) \end{gathered}$ | $\begin{gathered} 2 \\ 8 \\ (10) \end{gathered}$ |

Note: 1. On localised gradient which is steeper than range for rolling gradient (3-6\%)
2. For projected $5,000-7,000 \mathrm{vpd}$, Policy has 5 or 10 km spacing but generally at the lower end of projected AADT interval use 10 km spacing.
3. Regression analysis based on extrapolation from counters approx $1.2 \& 3.5 \mathrm{~km}$ downstream gave 13.5 km . From mathematical model, calculated 8.3 km downstream operational length.

Policy layouts are generally similar to the observed values. However, on mountainous road gradients such as for sites 6 e and 8 j , either closer frequencies for passing lanes or possibly at higher flows, crawler lanes may be required but this would have to be balanced against other factors such as cost, impact on landform and the duration of reduced level of service. At low flows ( $<5,000$ projected vpd) on flat gradients, the Policy layout uses $600-800 \mathrm{~m}$ short passing lanes, which may be slightly under-provision and therefore a longer length would be favoured. Shorter passing lengths may be appropriate, if on steeper gradients compared to downstream.

The projected AADT interval for most sites is based on $55 / 45 \%$ directional split and an assumed peak hour flow of $10.5 \%$ AADT (Approx $125^{\text {th }}$ percentile highest hour). Sites 4 j and 6 e are both on rural commuter routes. For site 4 j , a $65 / 35 \%$ directional split and assumed peak hour flow of $12 \%$ AADT (Approx $125^{\text {th }}$ percentile highest hour) was used. For site 6 e , a $55 / 45 \%$ directional split and assumed peak hour flow of $12 \%$ AADT was a better match to surveyed flows.

In order to help understand the passing characteristics for each passing lane and slow vehicle bay, a plot of percentage passing relative to one-way flow was generated for each counter location. Figure 4 shows the plot for the mid-point of each passing lane and slow vehicle bay.

## MEASUREMENT OF PASSING/OVERTAKING DEMAND

## Study Sites

A pilot study was undertaken by MWH NZ Ltd. into using Transit's traffic monitoring system (TMS) for assessing passing/overtaking demand on rural two-lane state highways. The pilot study area consisted of about 90 sites (almost 180 directional files) in the Waikato and Bay of Plenty regions, using MetroCount traffic data for one week in 2006.

## Determination of Headway

The study initially investigated the appropriate headway threshold for determining whether a vehicle was assumed to be following or travelling freely. Alternative headway thresholds were investigated ( $3.5,4.0,4.5,5.0$ seconds) based on the range of values used internationally. The speed distribution for the platooned and free vehicles over a sample of sites showed little effect in changing the assumed 'free' threshold. This lack of change is probably due to the vast majority of the number of platooned vehicles remaining unchanged across the threshold range.

However, the cumulative frequency of headways indicated a noticeable change in profile below the 4 second threshold. With a preference for adopting whole numbers and for a 'tight' criterion, the study recommended 4.0 seconds as the appropriate threshold for determining the percentage following.

## Percentage Following

Based on the 4 second threshold, graphs of the percentage following distribution were undertaken for each site. Figure 5 shows the plot of percentage following versus one-way flows for an example site on State highway (SH) 2. Figure 6 shows the plot of percentage following versus average Monday-Friday one-way flows for higher flow (up to 1400 vph ) sites on SH 1. An example of the technique was later applied to assess passing/overtaking demand on SH 1 south of Blenheim over the Christmas 2007/08 period, as illustrated in Figure 7.

A cubic curve was fitted to the data for one-way flows up to 600 vph, above which a linear fit appeared reasonable. For a given average weekday hourly flow, the variation in the observed percentage following appeared to decrease with higher flows, with the associated observation that there were no very high flow (> 900 vph one-way) sites, which also had high percentages of heavy vehicles. Inspection of these graphs indicated that the percentage following appears to be influenced more by the percentage of heavy vehicles rather than speed, although there are correlative effects involved.

Table 8 compares one-way flows, percentage following and percentage heavy vehicles for a randomly selected number of sites. For similar values of percentage heavy vehicles, the percentage following values increased as one-way flows increased. This observation is similar to surveyed data in the previous study but varies from mathematical modelling of operational length where the percentage of heavy traffic was not a significant variable. This difference may be due to the limited number of sites used in the Table 8 comparison or the randomly selected sites are inadvertently mainly on rolling or mountainous road gradients.

Table 8: Comparison Between Percentage Following \& Percentage Heavy Vehicles

| One-Way <br> Flow (vph) | $<\mathbf{1 0 \%}$ <br> HV (\%) | Percentage <br> Following (\%) | $\mathbf{1 0 - 2 0 \%}$ <br> HV (\%) | Percentage <br> Following (\%) | $\mathbf{> 2 0 \%}$ <br> HV (\%) | Percentage <br> Following (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{3 0 0}$ | $6-9$ | 35 | 19 | 52 | $20-23$ | 46,52 |
| $\mathbf{6 0 0}$ | $7-9$ | 55 | 16 | 70 | 21 | 65 |
| $\mathbf{9 0 0}$ | $7-9$ | 68 | 15 | 77 | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $\mathbf{1 2 0 0}$ | 7 | 76 | 11 | 81 | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |

## Speed

Table 9 compares speed, traffic flow and the percentage following values at two sites for different time periods. Higher traffic volumes (and higher proportion of heavy vehicles) does not directly relate to a reduced speed and an increase in percentage following. Road geometrics and the timing of peak heavy traffic relative to passenger vehicle peak periods may partly explain the speed difference between sites. Seasonal/weekend effects could also influence speed results for the same site, particularly at lower AADTs.

Table 9. Intra-Site Comparison of Speed, Flow \& Percentage Following

| Site | 27/82 AB | 27/82 AB | 28/9 AB | 28/9 AB | 28/9 AB | 28/9 AB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Date for Week (2006) | 25 June | 14 July | 1 Mar | 15 July | 23 Aug. | 7 Sept. |
| Speed Comparison (km/h) |  |  |  |  |  |  |
| Mean speed, all vehicles | 89.8 | 84.6 | 60.8 | 69.5 | 69.4 | 68.5 |
| Mean speed, free vehicles | 90.8 | 85.8 | 61.7 | 70.2 | 70.0 | 69.2 |
| Mean speed, platooned vehicles | 87.0 | 81.0 | 57.9 | 67.3 | 66.9 | 65.6 |
| Flow Comparison (vpd) |  |  |  |  |  |  |
| One-way ADT (7 days) | 1939 | 1857 | 1432 | 1423 | 1496 | 1434 |
| \%HV Monday to Sunday | 18.9 | 17.5 | 16.7 | 15.3 | 14.7 | 16.8 |
| \%HV Saturday | 8.6 | 7.1 | 8.8 | 5.3 | 7.6 | 8.1 |
| \%HV Sunday | 8.7 | 6.1 | 6.0 | 3.8 | 5.2 | 4.8 |
| Percent Following Comparison (\%) |  |  |  |  |  |  |
| Predicted M-F \% following, 150 vph | 29.4 | 30.3 | 37.5 | 35.6 | 29.7 | 33.4 |

The predicted percentage following is derived from the linear best fit line. The observed values vary with the highest weekday flows being about 120 vph one-way. The best fit line is based on a minimum 20 vph with $r^{2}$ varying from 0.85 to 0.94 .

For the SH 27 site (i.e. $27 / 82$ in A-B direction), there is a difference of about $5 \mathrm{~km} / \mathrm{h}$ in the speed statistics and about $1-2 \%$ in the percentage of heavy vehicles, which is probably not atypical. For the SH 28 site, the observed March speeds were slower by about $8-9 \mathrm{~km} / \mathrm{h}$. The SH 28 site recorded a higher percentage of heavy vehicles over the whole weekend during March 2006 (early autumn with daylight saving) than for other periods of the year.

SH 28 has a R3 cross section (approx 8.5 m total seal width) compared to SH 27, which has a R2 cross section (approx 10 m total seal width). SH 27 is part of a long-haul route with the proportion of heavy vehicles being more consistent throughout the year and a higher proportion of heavy vehicles would travel at night outside of peak traffic periods.

## Effect of Light Vehicles Towing

A further observation related to using combined percentage heavy vehicles and light towing vehicles (Transit New Zealand 2004) rather than only percentage heavy vehicles. As part of the study, a comparison of the percentage following at various telemetry sites was compared with percentage heavy vehicles (vehicle classes 3-13) and light vehicles towing (vehicle class 2) (Appendix A, Transit New Zealand 2004). Results suggested that the combined percentage of heavy vehicles and light towing vehicles may be a better explanatory variable for percentage following than percentage heavy vehicles alone.

## Changes to Traffic Monitoring Process

Recommended changes to Transit's traffic monitoring strategy, as well as the Traffic Monitoring System's (TMS) data processing, recording, analysis and reporting functions include:

- Telemetry dual loop sites are to record the four length bins for free and platooned vehicles separately.
- $\quad$ Some MetroCount 'Regular' devices are to be upgraded to 'Plus' devices so that seven days of vehicle-by-vehicle data can be recorded at least once a year at each TMS site (or other traffic counters upgraded or replaced to a similar level).
- $\quad$ The equipment \& storage capacity at continuous dual loop sites should be capable not only of recording length by headway for a week but also preferably vehicle-by-vehicle.
- $\quad$ The posted speed limit to be a field in TMS.


## FURTHER RESEARCH

Research on more sites would help to confirm other points within the Policy long-term framework and make the mathematical models more robust for predicting both the operational length and the difference between upstream and downstream percentage following. A more detailed determination of downstream road gradient rather than a standard mid-range value may improve the fit of the operational length model. Possibly, for determining downstream conditions, the New Zealand classification system for combined terrain may be a more useful parameter than road gradient, as it takes into account changes in both vertical gradient and horizontal alignment (Land Transport NZ 2006). Opposing flows should also be considered.

For further work on measuring passing/overtaking demand, the data could be subjected to statistical hierarchical clustering techniques to objectively determine site groupings. The resulting dendogram(s) could then be further inspected to help both identify key influences and quantify their separate effects on passing/overtaking demand. This approach would reduce the need for data intensive analysis.

## CONCLUSION

This research has helped to confirm the Policy's framework for long-term development of New Zealand's two-lane rural state highways. The framework will provide practitioners with an easy reference point for selection of an appropriate layout. However, the projected AADTs should be qualified by one-way flow values and the parameter of road gradient needs to reflect downstream overtaking conditions typical for that terrain. Some professional judgement is still required, such as a shorter passing length if sited on a steeper grade compared to downstream.

Based on six selected sites, downstream platooning effects (using two and four second headway criteria) were generally in agreement with the Policy's long-term framework. Increased frequency of passing facilities may be required in some mountainous locations (i.e. projected $>12,000 \mathrm{vpd}$ ) but operational effects would have to be balanced against landscape issues and the duration of reduced level of service. At lower flows (i.e. projected $<5,000 \mathrm{vpd}$ ) some passing lanes on flat locations may have to be slightly longer than the Policy's 600-800 m.

The methodology outlined for measuring passing/overtaking demand will help practitioners to assess demand on an objective basis. However, speed also needs to be considered. A four second headway criterion is appropriate for New Zealand state highway conditions. A cubic curve relationship was identified between percentage following and one-way traffic volumes. Measurement of passing/overtaking demand is currently data intensive and therefore more suited to one-off situations than widespread assessment of the entire network.

## DISCLAIMER

The opinions presented in this paper are the views of the authors and not necessarily the views of their employer organisations.

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## ERRATA

For paper on $23^{\text {rd }}$ ARRB Conference CD, Equation 1 uses 2.12. Within this paper, 212 is used to allow for changing to percentage values for DPF.

For paper on $23^{\text {rd }}$ ARRB Conference CD, the merge date for the New Zealand Transport Agency was originally 1 July but the official merge date was changed after submissions closed . Therefore, a merge date after 31 July is used within this paper. Acknowledgements have been changed from the New Zealand Transport Agency to Transit for consistency.

## APPENDICES

| Treatments and Measures |  | Passing and Overtaking Strategy Type |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Overtaking | Mainly overtaking | Passing \& overtaking | Passing |
|  | Overtaking sight improvements |  |  |  |  |
|  | Vegetation control, batter relocation | C | C | C | - |
|  | Pavement rehabilitation, realignment | C | C | C | - |
|  | Overtaking enhancements |  |  |  |  |
|  | Seal widening | P | P | C | - |
|  | Overtake at PLs or SVBs, configuration of PLs or SVBs | $\mathbf{P}^{1}$ | P1 | $\mathbf{P}^{1}$ | - |
| $\begin{aligned} & \text { 을 } \\ & \text { g } \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | Low-volume treatments ${ }^{2}$ |  |  |  |  |
|  | Shoulder widening or crawler shoulder | P1 | $\mathrm{C}^{1}$ | - | - |
|  | SVB or short PL | $\mathrm{C}^{1}$ | P1 | - | - |
|  | Moderate-volume treatments ${ }^{3}$ |  |  |  |  |
|  | Wide shoulder (special use requirement) | - | - | C | - |
|  | PLs in series | - | - | P | $\mathrm{P}^{4}$ |
|  | Crawler lanes | - | - | C | C |
|  | 2+1 lanes (subject to four-lane comparison) | - | - | - | $\mathrm{P}^{5}$ |
| 9 | Centreline treatments |  |  |  |  |
|  | Line markings | P | P | P | C |
|  | Gap separation | - | - | C | P |
|  | Central median cables | - | - | C | P |
|  | Roadside/edgeline treatments |  |  |  |  |
|  | Clear zone and shoulder run-off | P | P | P | P |
|  | Increased signs and markings | P | P | P | P |
|  | Wide profile markings | C | C | P | P |
|  | Local shoulder widening and/or chip seal | C | C | P | P |
|  | Cable or guard rails | C | C | C | C |
|  | Intersection treatments |  |  |  |  |
|  | OT zones/PLs with respect to intersections | P | P | P | P |
|  | Provision for through traffic | C | C | P | P |
|  | Intersection rationalisation | - | - | P | P |
| Supporting measures | Resource planning measures |  |  |  |  |
|  | Control of direct access onto SH | C | C | P | P |
|  | Submissions (plan docs, RC applications) | C | C | P | P |
|  | Encourage alternative District networks | C | C | C | C |
|  | New alignments | C | C | C | C |
|  | Education measures |  |  |  |  |
|  | Target audience | C | C | C | P |
|  | General public | C | C | C | C |
|  | Enforcement measures |  |  |  |  |
|  | Problem locations | C | C | C | P |
|  | General public | C | C | C | C |
|  | TDM measures |  |  |  |  |
|  | Alternative hours, routes or modes | C | C | C | P |
|  | ITS measures |  |  |  |  |
|  | Variable message signs with/without web cam | C | C | C | C |
|  | Speed cameras | C | C | C | C |
| NOTES: |  |  |  |  |  |
| $\mathrm{P}=\mathrm{pr}$ $1=0$ $3=\mathrm{m}$ l $5=\mathrm{pr}$ Not an or com | eferred option/s, C = consider if specific problem <br> ly if overtaking strategy is not viable. <br> derate-volume is typically projected $4,000-25,000 \mathrm{vpd}$. ferred on flat/rolling terrain, subject to comparison with four exclusive list, others may be added at a later date. mbination on a case-by-case basis. | 2 = low- volum <br> 4 = preferred -lanes. <br> than one prefer | is typically less th mountainous ter option for sam | n projected 5,0 in. <br> treatment/meas | consider on |

Figure 1. Tool Kit Of Options


Figure 2. Vehicle Classifier Layout For Surveys Of Passing Facilities


Figure 3. Percentage Following Distributions Based On 2 Seconds Headway Criterion



Figure 4. Comparison Of Percentage Passing At Mid-Point Of Each Study Site


Figure 5. Plot Of Percentage Following Versus One-Way Flow For An Example Site


Figure 6. Plot Of Percentage Following Versus OneWay Average Mon-Fri Flow For SH 1 Sites
(Based on 4 seconds Headway Criterion)

## All sites:

Key for the first letter, speed for all vehicles A: <68 km/h; B: 68-78, C: 78-88; D: >=88 km/h Interval sites WADT, Mon-Fri \%HV, mean speed all vehs, Site id
Individual vehicles sites Site id, mean free speed/ lead veh speed, M-S \%HV


Figure 7. Plot Of Percentage Following Versus One-Way For SH 1S Blenheim South site

